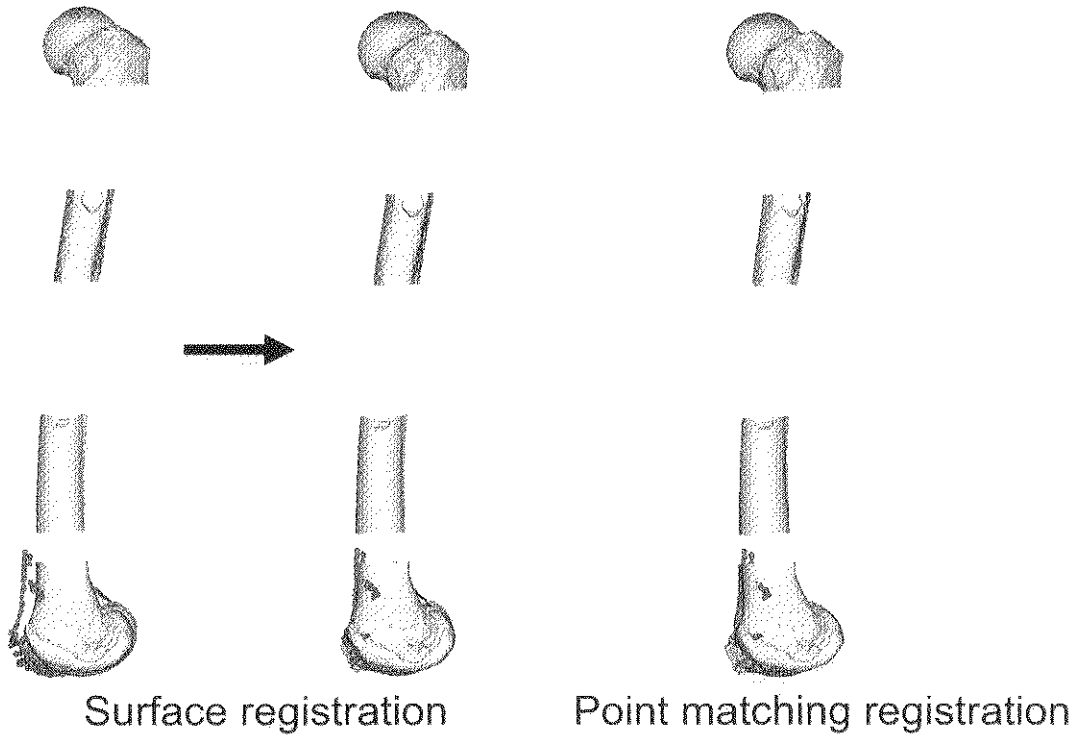
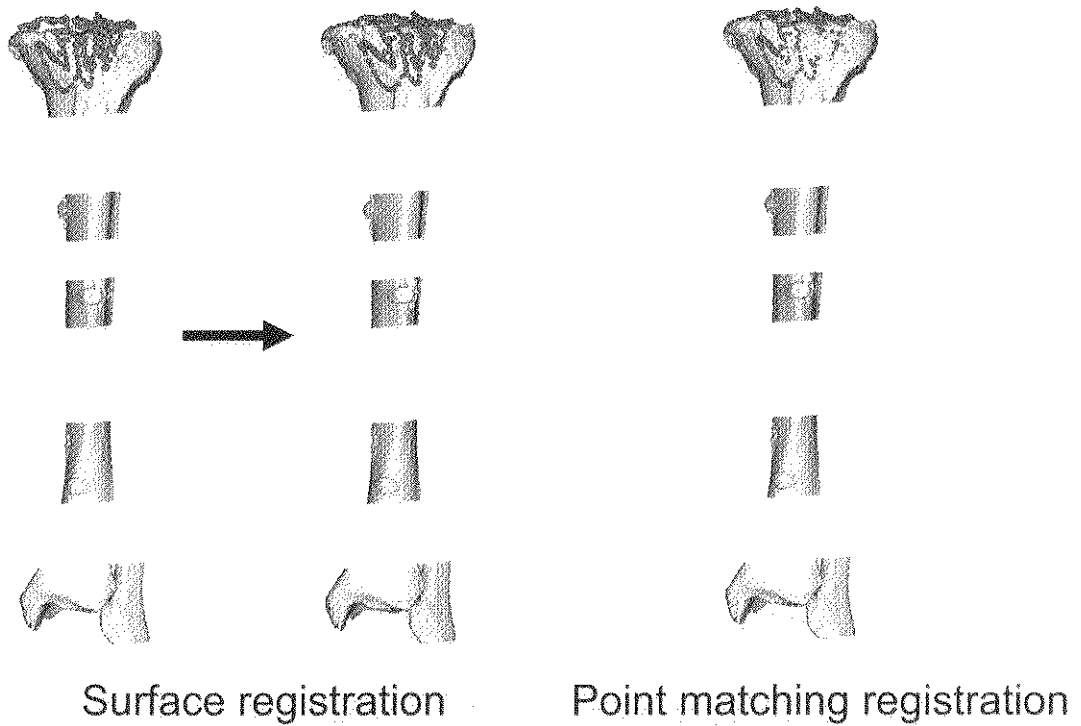


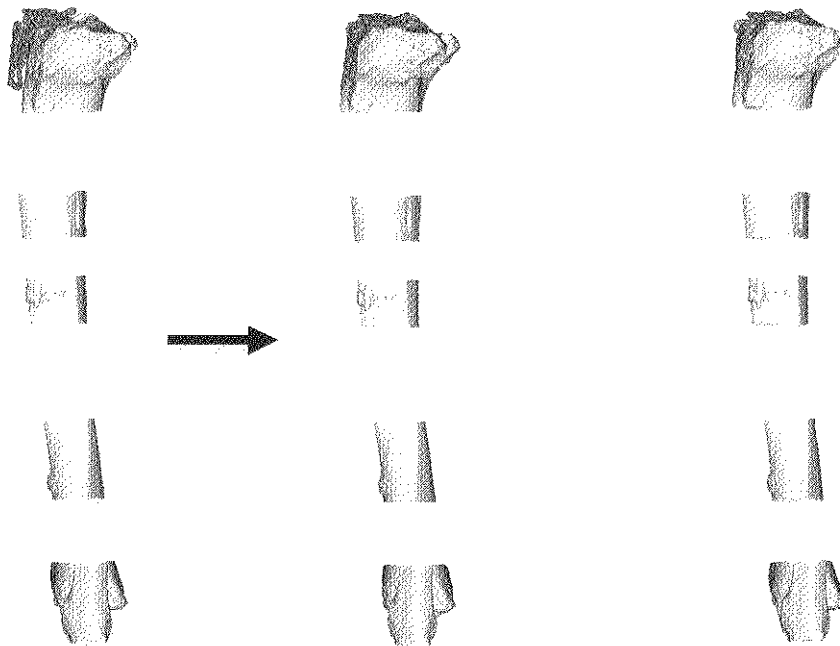
## Femur (Side view)



## Tibia (Front view)



## Tibia (Side view)



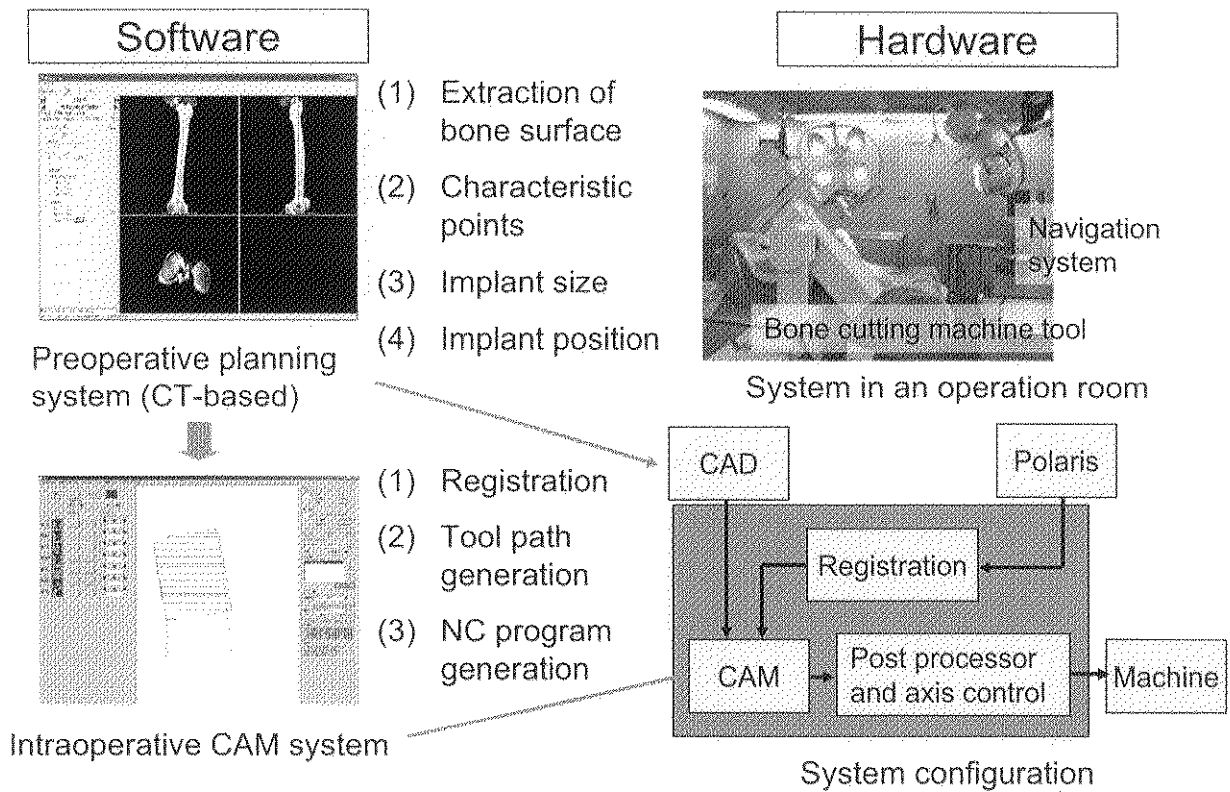
Surface registration

Point matching registration

## Coordinate system transformation

- The data to control the bone cutting machine tool is generated as follows: 
$${}^F T_A = {}^B T_A {}^C T_B {}^D T_C {}^E T_D {}^F T_E$$
- ${}^n T_m$ : Transformation from coordinate systems  $m$  to  $n$ .
- $A$ : Local coordinate frame of the artificial joint, which is fixed to each cut surface: The cutting areas for the femur and tibia are described with reference to  $A$ .
- $B$ : Artificial joint coordinate frame
- $C$ : Preoperative planning coordinate frame: The position of the artificial knee joint, feature points and the shape of femur and tibia are presented with reference to  $C$ .
- $D$ : Bone coordinate frame
- $E$ : Static coordinate frame
- $F$ : Bone cutting machine tool coordinate frame

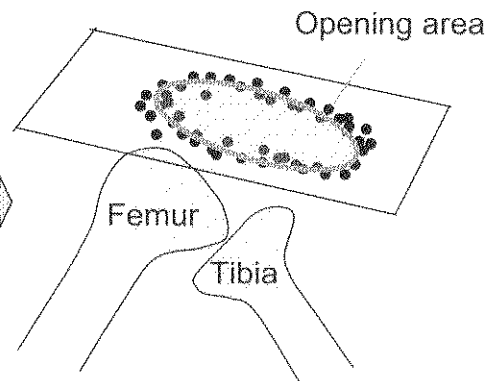
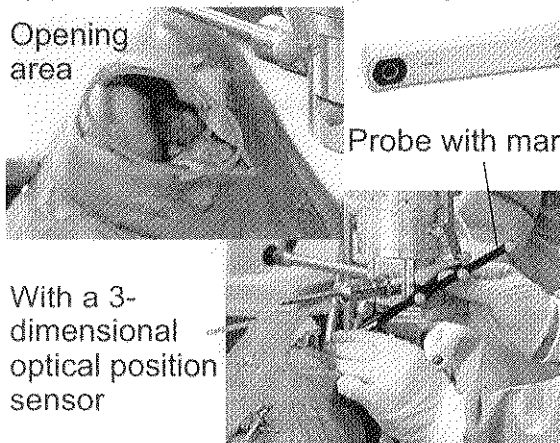
# System construction



## Toolpath generation: Step 1

### Modeling of knee joint

#### (1) Measurement of opening area



The border of the area is measured as the points for the opening plane.

Regression analysis is used for measured data  $\bar{P}_i (i=1, \dots)$ ,

$$J(a, b, c) = \sum (z_i - ax_i - by_i - c)^2$$

$$\frac{\partial J}{\partial a} = 0, \frac{\partial J}{\partial b} = 0, \frac{\partial J}{\partial c} = 0$$

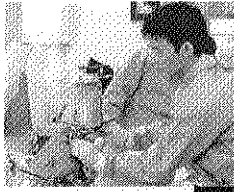
is calculated

A plane  $z = ax + by + c$  is obtained.

#### (2) Measurement of obstacles

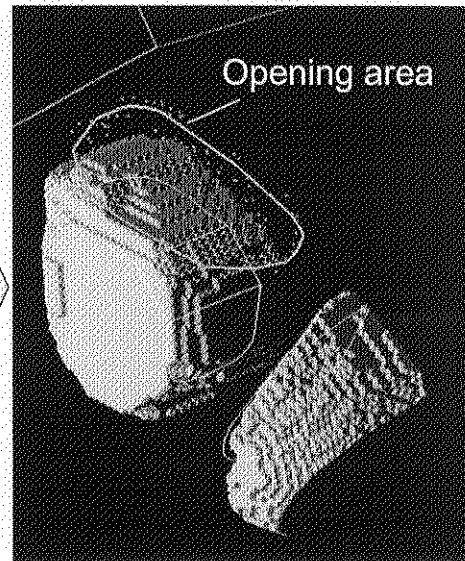
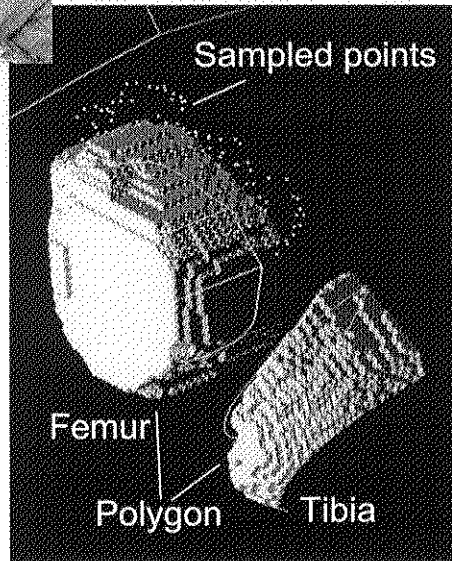
Area which cutting tool should not contact (soft tissue, nerves, vessels, etc.) is measured and calculated.

# Measurement of opening area



Sampling

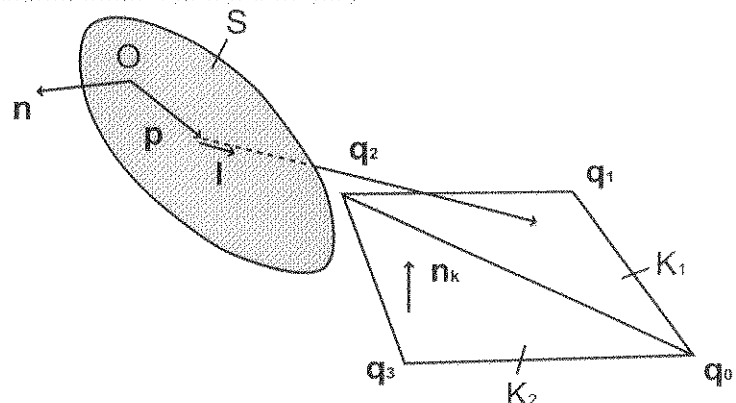
Calculation of opening area



## Toolpath generation: Step2(1)

### Calculation of the initial cutting tool posture

- The machinable area is calculated at a given cutting tool attitude utilizing the cross detection of the cutting tool vector and the target plane.
- The resection plane is divided into the triangle patches  $K_i$ .
- Vertex vectors are set  $q_i$ .



A local coordinate system  $S$  is set on the opening area.

Triangle patch  $K_i$  can be presented as

$$(1-u-v)\vec{q}_0 + u\vec{q}_1 + v\vec{q}_2$$

$$0 < u, v < 1$$

$\vec{p} = (x \ y \ z)^T$ : offset vector from the origin

$\vec{l} = R(\theta, \phi)(0 \ 0 \ 1)^T$ : attitude vector

The cutting tool vector can be presented as

$$\vec{p} + t \cdot \vec{l}$$

## Toolpath generation: Step2(2)

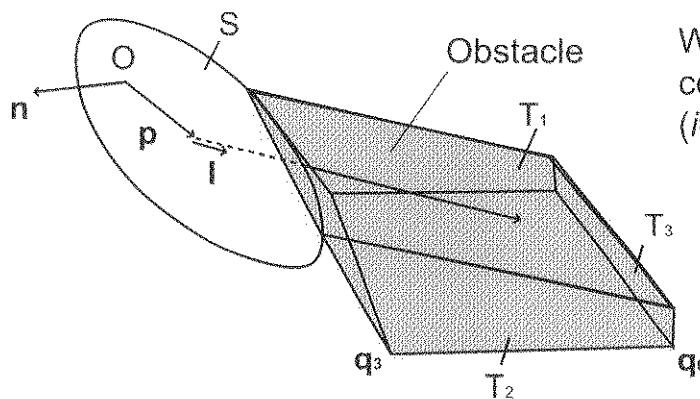
### Calculation of the initial cutting tool posture

The following equation detects whether the patch is machinable:

$$\begin{pmatrix} -\vec{l} & (\bar{q}_1 - \bar{q}_0) & (\bar{q}_2 - \bar{q}_0) \end{pmatrix} \begin{pmatrix} u \\ v \end{pmatrix} = (\bar{p} - \bar{q}_0)$$

(Equation of Tomas Moller)

The detection is executed for all patches.



When it is machinable, the collision with interferences  $T_i$  ( $i=1, \dots$ ) is checked.

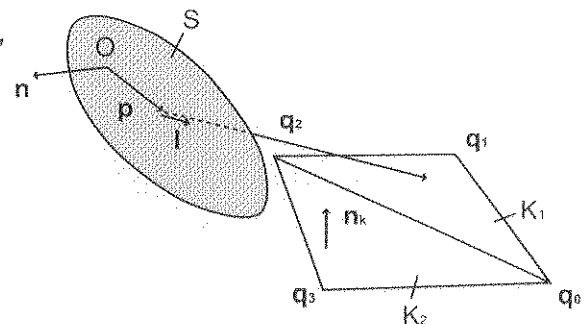
## Toolpath generation: Step2(3)

### Calculation of the initial cutting tool posture

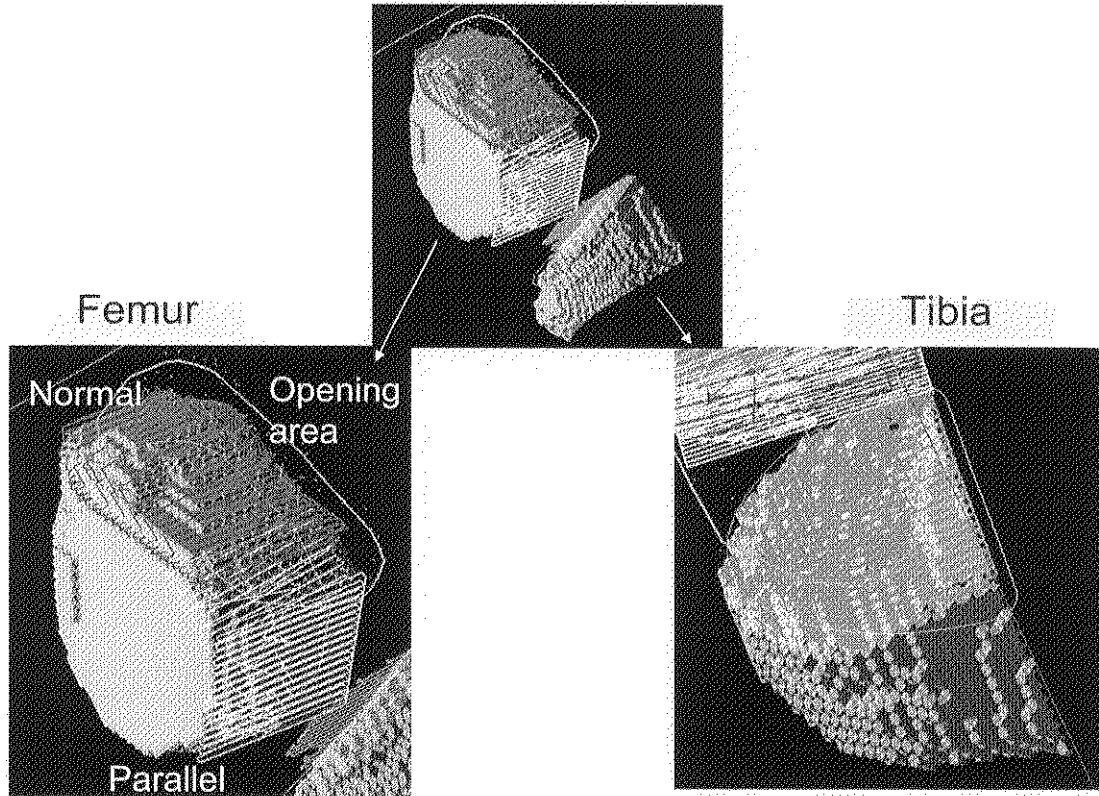
- The offset vector  $\mathbf{p}$  is varied on the opening plane with the parameter of the tool attitude  $\mathbf{l}$ , and the machinable area is calculated on the triangle patch  $K_i$ .
- An attitude  $\mathbf{l}$  to maximize the evaluation function is selected as the initial tool posture.

$$E(\vec{l}, \vec{p}) = \begin{cases} 1 & \text{(without collision)} \\ 0 & \text{(with collision)} \end{cases}$$

$$J(\vec{l}) = \sum_{k_1}^{k_p} \int E(\vec{l}, \vec{p}) dx dy \quad x, y, \vec{p} \in S$$

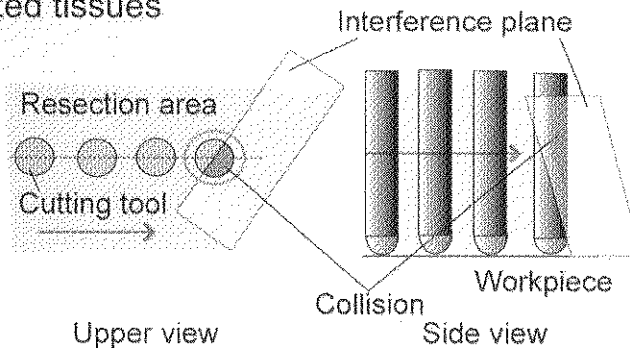


# Calculation of cutter location

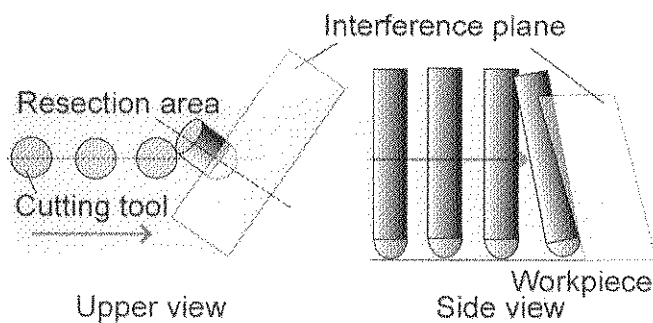


# Collision avoidance

Interference with prohibited tissues are checked.



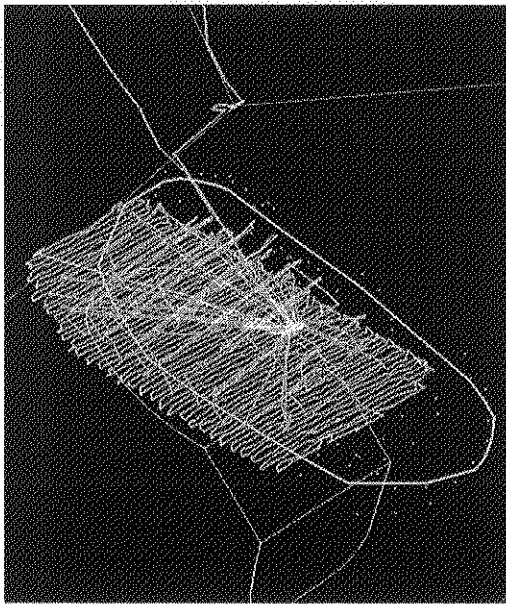
Strategy of avoidance



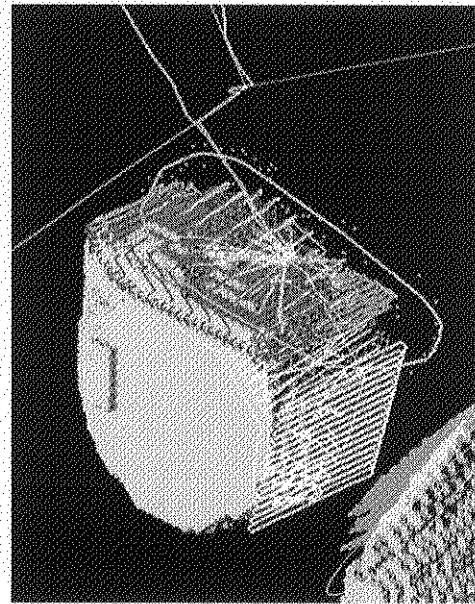
- Interference is avoided with a minimal change of the cutting tool attitude
- The avoidance direction is equal to the normal vector of the interference plane.

# Toolpath generation: Step3

Trajectory



Cutter location and trajectory



## Concept of toolpath generation

### Requirements

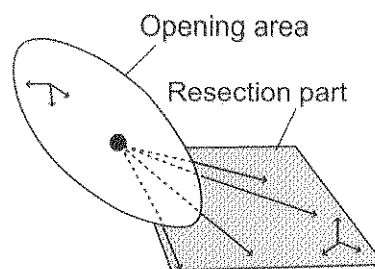
- (1) Less invasiveness
- (2) Accuracy
- (3) Precision
- (4) Safety



### Strategy

- (1) Short incision length
- (2) Less attitude change

### Strategy 1: Incision length minimization

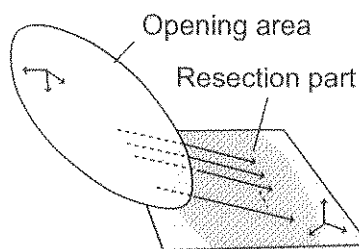


Short incision



Attitude of the cutting tool is changed actively

### Strategy 2: Not changing the tool attitude



Less attitude change



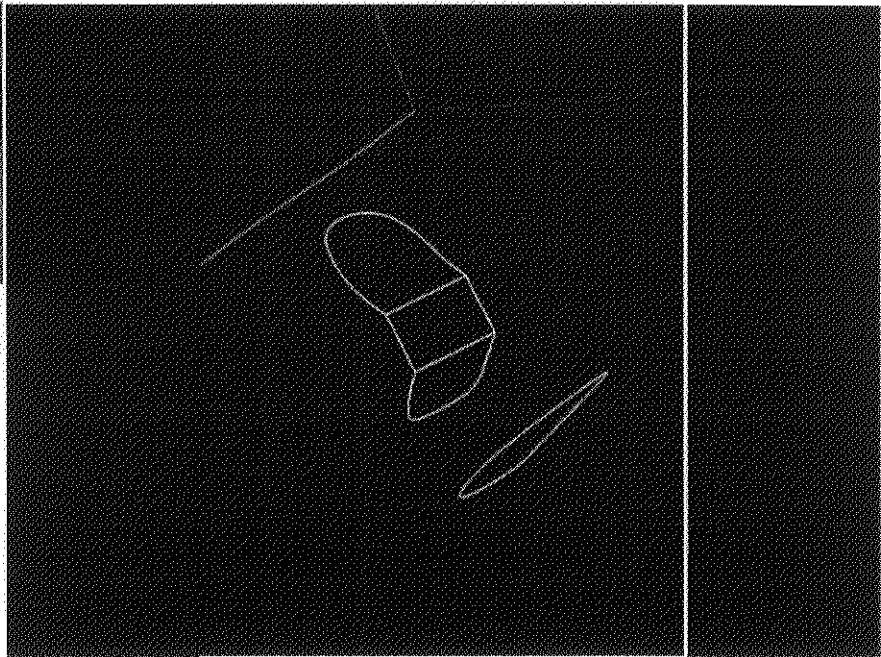
Easy to predict the attitude and position of the tool

# Prototype of proposed method: video

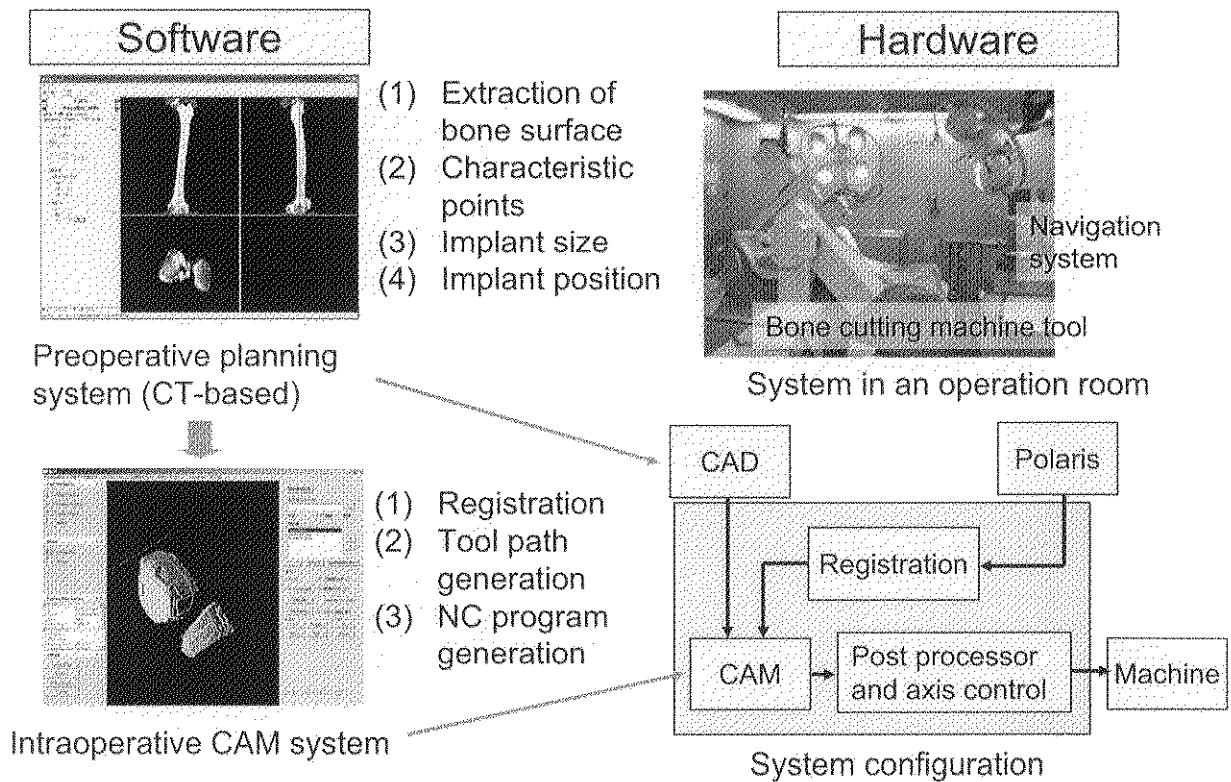
Setting plane of UKA



Flow of toolpath generation

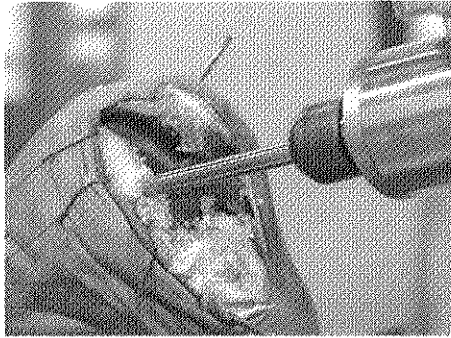


## Implementation: overview of the system

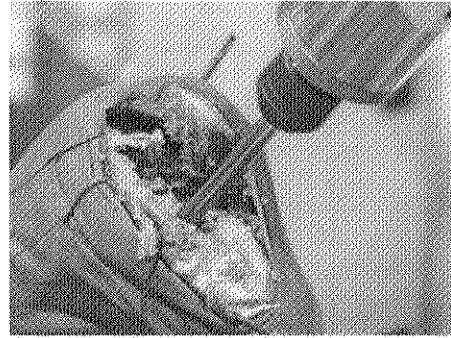




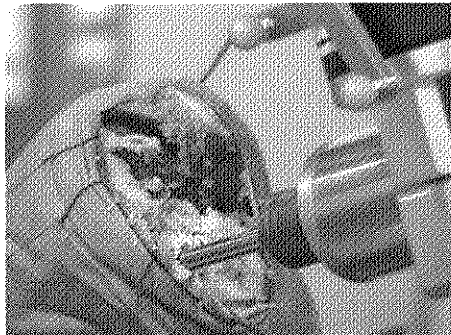
## Cutting experiment with a cadaver



Distal plane



Posterior slope



Posterior plane

### Cutting Conditions:

Cutting speed: 125.6 m/min

Feed speed: 400 mm/min

Spindle speed: 5,000 rpm

Depth of cut: 3 mm

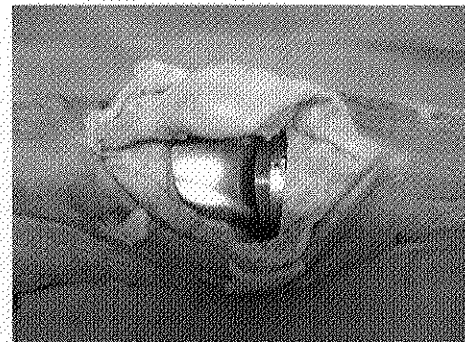
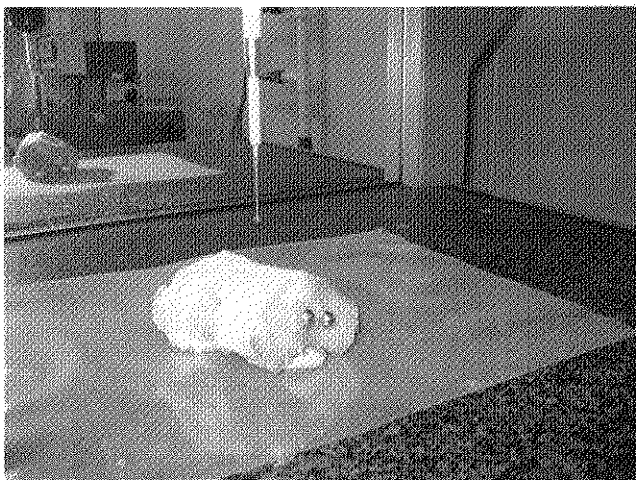
Cutting tool: end mill, biocompatible metal

Number of tooth: 4

Cutting tool diameter: 8 mm

Incision length: 100 mm

## Measurement using a CMM



## Experimental result: Analysis of cutting result

### Angular error

Axis	Error (deg.)
Epicondyle axis	1.8
Load axis (normal to ③)	0.7

### Position error of planes

Plane	Distance between local origin point and CAM calculated (mm)
Distal	0.847
Posterior	0.991

### Angle error between adjacent planes

Evaluated plane	Planned (deg.)	Measured (deg.)	Error (deg.)
①-②	135.0	134.2	0.8
②-③	120.0	120.3	0.3



## Conclusions

- A medical CAD/CAM system has been developed to assist a minimally invasive knee arthroplasty.
  - In particular, a method was proposed to measure the positions of soft tissues, and to avoid any collision with these obstacles.
  - The system has a feature to provide safe operation by not changing the posture of the bone cutting machine tool during the surgical operation.
- A multi-axis bone cutting machine tool with safety, sterilization and irrigation capability was implemented.
- Minimally invasive cutting experiment for a cadaver was performed using the developed system.
  - The angular error from the load axis of the femur was less than 2.0 deg.
  - The maximum angle error of adjacent planes was approximately 1.0 deg.
  - The position error of the planes was less than 1 mm.
  - The incision length was reduced to 100 mm.